## Engr 154 Exam Note Sheet updated s20

2/2 Rectilinear Motion	2/5 Normal and Tangential Coordinates ( <i>n</i> - <i>t</i> )
Fundamental Kinematics Equations:	$\underline{\mathbf{v}} = v \mathbf{e}_{\mathbf{t}} = \rho \dot{\beta} \mathbf{e}_{\mathbf{t}}$
(1) $v = \frac{ds}{dt} = \dot{s}$	$\mathbf{\underline{a}} = \mathbf{\underline{v}} = a_t \mathbf{e_t} + a_n \mathbf{e_n} = \dot{v} \mathbf{e_t} + \left(\frac{v^2}{2} \left  \rho \dot{\beta}^2 \right  v \dot{\beta} \right) \mathbf{e_n}$
(2) $a = \frac{dv}{dt} = \dot{v} = \frac{d^2s}{dt^2} = \ddot{s}$	
(3)  v  dv = a  ds	Circular motion:
When <i>a</i> is <u>constant</u> :	$ ho  ightarrow r$ , $\dot{eta}  ightarrow \dot{ heta}$ ;
$v = v_o + at$	$v = r\dot{\theta}$
$s = s_o + v_o t + \frac{1}{2}at^2$	$a_t = \dot{v} = r\dot{\theta}, \qquad a_n = v^2/r = r\dot{\theta}^2 = v\dot{\theta}$
$v^2 = v_o^2 + 2a(s - s_o)$	
If <i>a</i> is not constant, use one of the fundamental kinematic equations and appropriately integrate/differentiate.	
2/3 Plane Curvilinear Motion	$2/6$ Polar Coordinates ( <i>r</i> - $\theta$ )
$d\mathbf{r}$	$\mathbf{r} = r\mathbf{e}_{\mathbf{r}}$
$\underline{\mathbf{v}} = \frac{1}{dt} = \underline{\mathbf{F}}$	$\mathbf{v} = v_r \mathbf{e_r} + v_\theta \mathbf{e_\theta} = \dot{r} \mathbf{e_r} + r \dot{\theta} \mathbf{e_\theta}$
$\underline{\mathbf{a}} = \frac{d\mathbf{v}}{dt} = \underline{\mathbf{v}}$	$\mathbf{a} = a_r \mathbf{e_r} + a_\theta \mathbf{e_\theta} = (\ddot{r} - r\dot{\theta}^2)\mathbf{e_r} + (r\ddot{\theta} + 2\dot{r}\dot{\theta})\mathbf{e_\theta}$
2/4 Rectilinear Coordinates	2/8 Relative Motion
$\mathbf{r} = \mathbf{r}\mathbf{\hat{i}} + \mathbf{v}\mathbf{\hat{i}}$	$\mathbf{r}_{1} = \mathbf{r}_{2} + \mathbf{r}_{1}$
$\mathbf{v} = \dot{\mathbf{r}} = \dot{x}\mathbf{i} + \dot{y}\mathbf{j}$ $\mathbf{v} = \dot{\mathbf{r}} = \dot{x}\mathbf{i} + \dot{y}\mathbf{i} = v_x\mathbf{i} + v_y\mathbf{i}$	$\frac{1}{A}$ $\frac{1}{B}$ $\frac{1}{A/B}$
$\mathbf{a} = \dot{\mathbf{v}} = \ddot{\mathbf{r}} = \ddot{x}\hat{\mathbf{i}} + \ddot{y}\hat{\mathbf{j}} = a_x\hat{\mathbf{i}} + a_y\hat{\mathbf{j}}$	$\underline{\mathbf{v}_{A}} = \underline{\mathbf{v}_{B}} + \underline{\mathbf{v}_{A/B}}$
Speed (magnitude of velocity): $v = \sqrt{v_x^2 + v_y^2}$	$\underline{\mathbf{a}_{\mathbf{A}}} = \underline{\mathbf{a}_{\mathbf{B}}} + \underline{\mathbf{a}_{\mathbf{A}/\mathbf{B}}}$
Direction of motion: $\tan \theta = \frac{v_y}{v_y}$	
Acceleration $a = \sqrt{a_x^2 + a_y^2}$	
Projectile Motion	2/9 Constrained Motion
initial position ( $x_0$ , $y_0$ ), initial velocity $v_0$ :	Cable/Pulley Systems: write cable length(s) – or other
$a_x = 0$ $a_y = -g$	dimensions that remain constant – in terms of
$v_x = v_{o,x} \qquad \qquad v_y = v_{o,y} - gt$	variable distances. Lable length <i>L</i> is constant; its derivative is:
$x = x_o + v_{o,x}t$ $y = y_o + v_{o,y}t - \frac{1}{2}gt^2$	$\dot{L} = 0 = derivatives of variable distances$
Also: $(v_y)^2 = (v_{0y})^2 - 2g(y - y_0)$	Alternate: Use differential movement <i>ds</i> of a point on
	cable, and how <i>ds</i> promulgated to various points on
	the cable/around pulleys, etc. <i>v=ds/dt</i> .
The same vector can be represented in different	

coordinate systems (x-y), (n-t),  $(r-\theta)$ .

Lay out the same vector in different coordinate systems. Use vector geometry/trigonometry to determine sides of the vector triangle in different coordinate systems.

$$\underline{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} = r\underline{\mathbf{e}_{\mathbf{r}}}$$
  

$$\underline{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} = v\underline{\mathbf{e}_{\mathbf{t}}} = v_r\underline{\mathbf{e}_{\mathbf{r}}} + v_\theta\underline{\mathbf{e}_{\theta}}$$
  

$$\underline{\mathbf{a}} = a_x\hat{\mathbf{i}} + a_y\hat{\mathbf{j}} = a_t\underline{\mathbf{e}_{\mathbf{t}}} + a_n\underline{\mathbf{e}_{\mathbf{n}}} = a_r\underline{\mathbf{e}_{\mathbf{r}}} + a_\theta\underline{\mathbf{e}_{\theta}}$$

The magnitude of a vector is the same in any coordinate system, e.g., the magnitude of the velocity and acceleration are, respectively:

$$v = \sqrt{v_x^2 + v_y^2} = v_t = \sqrt{v_r^2 + v_\theta^2}$$
$$a = \sqrt{a_x^2 + a_y^2} = \sqrt{a_t^2 + a_n^2} = \sqrt{a_r^2 + a_\theta^2}$$

## **Chapter 3: Kinetics of Particles**

3/4 Rectilinear Motion	3/7 Potential Energy
$\sum \mathbf{F} = m\mathbf{a}$	$V_g = mgh$ $\Delta V_g = mg(\Delta h)$
$\sum_{i=1}^{n} \frac{1}{m_{i}}$	$V_e = \frac{1}{2}kx^2$ $\Delta V_e = \frac{1}{2}k(x_2^2 - x_1^2);$ x=displ. of spring
$\Sigma F_{\chi} = m u_{\chi}  \Sigma F_{y} = m u_{y}  \Sigma F_{z} = m u_{z}$	from equilib.
$\left \Sigma\underline{\mathbf{F}}\right  = \sqrt{(\Sigma F_x)^2 + (\Sigma F_y)^2 + (\Sigma F_z)^2}$	Work-Energy Equation
	mechanical energy $E = T + V_a + V_a$
$a = \sqrt{a_x^2 + a_y^2 + a_z^2}$	$U_{nc} = \Delta T + \Delta V_{c} + \Delta V_{c} = \Delta E$
,	$E_{1} = E_{1} + U_{nc}$
3/5 Plane Curvilinear Motion	3/8 Linear Impulse and Linear Momentum
Rectangular	$\mathbf{G} = m\mathbf{v}$
$\Sigma F_x = ma_x$ $a_x = \ddot{x}$	$\Sigma \mathbf{F} = \dot{\mathbf{G}} = m\dot{\mathbf{v}}$ ; (external forces)
$\Sigma F_y = ma_y$ $a_y = \ddot{y}$	$\Sigma F_{x} = \dot{G}_{x} = m\dot{v}_{x};  \Sigma F_{y} = \dot{G}_{y};  \Sigma F_{z} = \dot{G}_{z}$
Normal-Tangential	$\int \int f_2 dx $
$\Sigma F_n = ma_n \qquad a_n = v^2/\rho = \rho\dot{\beta}^2 = v\dot{\beta}$	$\Sigma \mathbf{\underline{F}} dt = \Delta \mathbf{\underline{G}} = m \Delta \mathbf{\underline{v}}$
$\Sigma F_t = ma_t$ $a_t = \dot{\nu}$	$J_{t_1}$
Polar $\Sigma E = m z$ $z = \ddot{m} z + \dot{a} \dot{a}^2$	$\underline{\mathbf{G}}_2 = \underline{\mathbf{G}}_1 + \int \Sigma \underline{\mathbf{F}}  dt$
$\Sigma F_r = ma_r \qquad a_r = r - r\theta^2$	Collisions: <b>G</b> of system conserved if no external force.
$\frac{2I_{\theta} - I_{\theta} u_{\theta}}{2/6}$ Work and Kinotic Energy	2/0 Angular Impulse and Angular Momentum
$S/O$ work done by force <b>F</b> during displacement $d\mathbf{r}$	$H = r \times mv$
$dU = \mathbf{F} \cdot d\mathbf{r}$	$\frac{\mathbf{H}_0}{\mathbf{H}_0} = \frac{\mathbf{I}}{\mathbf{I}} \wedge \frac{\mathbf{I}}{\mathbf{V}}$
Work done by force <b>E</b> during finite motion (1) to (2):	$\frac{\mathbf{n}_0}{\mathbf{n}_0} = m(yv_z - zv_y)\mathbf{I} + m(zv_x - xv_z)\mathbf{J} + m(xv_y - yv_x)\mathbf{K}$
$\int_{-\infty}^{2} \int_{-\infty}^{2} \left( \frac{1}{2} + \frac{1}{2} +$	$\Sigma \underline{\mathbf{M}}_{O} = \underline{\dot{\mathbf{H}}}_{O} = \underline{\mathbf{r}} \times m \underline{\dot{\mathbf{v}}}$ (external moments)
$U_{1-2} = \int_{1} \underline{\mathbf{F}} \cdot d\underline{\mathbf{r}} = \int_{1} (F_{x} dx) + (F_{y} dy) + (F_{z} dz)$	$\Sigma M_{Ox} = \dot{H}_{Ox};  \Sigma M_{Oy} = \dot{H}_{Oy};  \Sigma M_{Oz} = \dot{H}_{Oz}$
Work done by constant force $\underline{\mathbf{P}}$ moving distance $\Delta s$	$\int_{-\infty}^{t_2} t = \Delta \mathbf{I}$
$H = \int_{-\infty}^{2} \mathbf{F} \cdot d\mathbf{r} = P \Delta \mathbf{s}$	$\int_{t_1} \underline{\Sigma} \underline{\mathbf{M}}_O  dt = \underline{\Delta} \underline{\mathbf{H}}_O$
$O_P = \int_1 \frac{\mathbf{r}}{\mathbf{u}}  \mathbf{u}  \mathbf{L} = I  \Delta S$	$\begin{pmatrix} t_2 \\ t_2 \end{pmatrix} = \begin{pmatrix} t_2 \\ t_2 \end{pmatrix}$
Work done by spring force on object	$\left(\underline{\mathbf{H}}_{o}\right)_{2} = \left(\underline{\mathbf{H}}_{o}\right)_{1} + \int_{t_{1}} \Sigma \underline{\mathbf{M}}_{O} dt$
$U_s = \int_{-\infty}^{\infty} \mathbf{E} \cdot d\mathbf{r} = -\frac{1}{2}k(x_2^2 - x_1^2) = \frac{1}{2}k(x_1^2 - x_2^2)$	Collisions: $\underline{\mathbf{H}}_{o}$ of system conserved if no external moment.
J <sub>1</sub> Z Z Work done by gravity (near earth)	2/421
$\int_{-\infty}^{2}$	3/12 Impact
$U_g = \int_1 \underline{\mathbf{F}} \cdot d\underline{\mathbf{r}} = -mg(y_2 - y_1) = mg(y_1 - y_2)$	$12'_{1} - 12'_{1}$
Work done by gravity (far from earth)	$e = \frac{v_2 - v_1}{v_1 - v_2}$
$U_{q} = \int_{-\infty}^{\infty} \mathbf{F} \cdot d\mathbf{r} = Gm_{e}mR^{2}\left(\frac{1}{m} - \frac{1}{m}\right)$	Only affects velocity <u>normal</u> to impact plane.
$J_1$ $(T_2 T_1)$ Work-Kinetic Energy Theorem	Collisions
$IL_{r,s} = \int_{-\infty}^{\infty} \mathbf{F} \cdot d\mathbf{r} = \int_{-\infty}^{\infty} (F_{r} ds) = \int_{-\infty}^{\infty} (ma_{r} ds) =$	<b>G</b> of system conserved if no net external force on system
$\int_{1-2}^{2} (mudu) - \frac{1}{2}m(v^{2} - v^{2}) - T = T.$	$\underline{\mathbf{H}}_{o}$ of system conserved if no net external moment
$J_1(muu) = {}_2m(v_2 - v_1) = r_2 - r_1$ Work done by all forces on mass equals $\Lambda T_1$	<u>Elastic</u> : objects bounce; energy conserved: $T_i = T_f$
$II_{1-2} = \Lambda T$	Inelastic: objects stick; energy not cons'd: $\mathbf{v}_1' = \mathbf{v}_2'$
Power	Impact: chiests hounces energy not cons'd. $a = \frac{v'_2 - v'_1}{v'_1 - v'_1}$
$P = \mathbf{F} \cdot \mathbf{y} = \frac{dU}{dU}$	$\frac{\text{impact}}{v_1 - v_2}$
$\frac{1}{1} - \underline{\mathbf{r}} \cdot \underline{\mathbf{v}} - \frac{1}{dt}$	Units
Ethciency:	Work: $1 I = 1 N \cdot m$
$e = \frac{P_{out}}{P_{in}}$ Overall Efficiency: $e = e_m e_e e_t$	Energy: 1 W= 1 J/s; 1 hp = 550 ft-lb/sec = 746 W

## **Chapter 5: Kinematics of Planar Motion**

## 5/2 Rotation

Fundamental Kinematics Equations – Angular Motion (analogous to linear motion)

(1) 
$$\omega = \frac{d\theta}{dt} = \dot{\theta}$$
  
(2)  $\alpha = \frac{d\omega}{dt} = \dot{\omega} = \frac{d^2\theta}{dt^2} = \ddot{\theta}$   
(3)  $\omega d\omega = \alpha \, d\theta$ 

When  $\alpha$  is <u>constant</u>:

$$\omega = \omega_o + \alpha t$$
  

$$\theta = \theta_o + \omega_o t + \frac{1}{2}\alpha t^2$$
  

$$\omega^2 = \omega_o^2 + 2\alpha(\theta - \theta_o)$$

If  $\alpha$  is not constant, use one of the fundamental kinematic equations and appropriately integrate/differentiate.

Vector Algebra for motion of Point A about a fixed axis
through Point O (relative to Point O)

$$\underline{\mathbf{v}}_{\underline{A}} = \underline{\mathbf{\omega}} \times \underline{\mathbf{r}} = \omega r \underline{\mathbf{e}}_{\underline{t}} \qquad \underline{\mathbf{r}} \text{ is } \textit{from } \text{Pt 0 } \textit{to } \text{Pt } A.$$
$$\underline{\mathbf{a}}_{\underline{A}} = \underline{\mathbf{a}}_{\underline{t}} + \underline{\mathbf{a}}_{\underline{n}} = \alpha r \underline{\mathbf{e}}_{\underline{t}} + \omega^2 r \underline{\mathbf{e}}_{\underline{n}}$$
$$= \underline{\alpha} \times \underline{\mathbf{r}} + \underline{\omega} \times (\underline{\omega} \times \underline{\mathbf{r}})$$

5/3 Absolution Motion

• Define geometry in terms of linear & angular positions.

• Take derivative to relate linear & angular velocities.

• Take derivative to relate linear & angular accelerations. e.g., in a triangle,

$$y = x tan \theta \dots \dot{y} = \dot{x} tan \theta + x sec^2 \theta(\dot{\theta})$$

5/4 Relative Velocity, 5/6 Relative Acceleration  $\underline{\mathbf{v}_{A}} = \underline{\mathbf{v}_{B}} + \mathbf{v}_{A/B} = \underline{\mathbf{v}_{B}} + \underline{\boldsymbol{\omega}_{AB}} \times \mathbf{r}_{A/B}$  $\underline{\mathbf{a}_{A}} = \underline{\mathbf{a}_{B}} + \underline{\mathbf{a}_{A/B}} = \underline{\mathbf{a}_{B}} + \left(\underline{\mathbf{a}_{A/B}}\right)_{t} + \left(\underline{\mathbf{a}_{A/B}}\right)_{n}$ 

Generally, the vectors are broken up into x- and ycomponents. Be careful about directions!

 $= \mathbf{a}_{B} + \alpha r \mathbf{e}_{t} + \omega^{2} r \mathbf{e}_{n}$ 

5/5 Instantaneous Center of Zero Velocity • Construct lines perpendicular to two (or more) velocities on a rigid body

• Intersection of constructed lines is ICOZV (Pt *C*)

• Velocity of any Pt A on the rigid body is equal in magnitude to :  $v_A = \omega r_{A/O}$  and is perpendicular to the vector from Pt. *O* to Pt. *A*; i.e.,:  $\mathbf{v}_A = \underline{\boldsymbol{\omega}} \times \mathbf{r}_{A/O}$ 

6/2 General Plane Motion Equations  $\Sigma \mathbf{F} = m\mathbf{a}$ 

$$\Sigma F_x = ma_x \quad \Sigma F_y = ma_y$$
$$|\Sigma \underline{\mathbf{F}}| = \sqrt{(\Sigma F_x)^2 + (\Sigma F_y)^2}$$
$$a = \sqrt{a_x^2 + a_y^2}$$

Assuming rotation only about *z*-axis, only need use scalar version of moment. etc.

Moments about Center of Mass Pt. G:

 $\sum M_G = I_G \alpha$ Moments about non-accelerating or fixed Point O:  $\sum M_0 = I_0 \alpha$ Moments about arbitrary Point *P*:

$$\sum M_P = I_G \alpha + m a_G d$$

where  $a_G$  is the magnitude of acceleration of C.O.M., and *d* is the perpendicular distance from point P to the line of action of  $a_G$ 

Moments about arbitrary Point *P*:

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$$\sum \underline{\mathbf{M}_{\mathbf{P}}} = I_{P}\underline{\alpha} + \underline{\rho_{G}} \times m\underline{\mathbf{a}_{\mathbf{p}}}$$
where:  

$$\underline{\alpha} \text{ is the vector angular acceleration,}$$

$$\underline{\rho_{G}} \text{ is vector position } \mathbf{from} \text{ Pt. } P \text{ to Pt. } G$$

$$\underline{\mathbf{a}_{\mathbf{p}}} \text{ is vector acceleration of Pt. P}$$
6/3 Translation  

$$\sum \underline{\mathbf{F}} = m\underline{\mathbf{a}} \quad ; \quad \sum M_{G} = 0$$
6/4 Fixed-Axis Rotation  

$$\sum \underline{\mathbf{F}} = m\underline{\mathbf{a}} \quad ; \quad \sum M_{G} = I_{G}\alpha \quad ; \quad \sum M_{O} = I_{O}\alpha$$
6/5 General Motion  

$$\sum \underline{\mathbf{F}} = m\underline{\mathbf{a}} \quad ; \quad \sum M_{G} = I_{G}\alpha \quad ; \quad \sum M_{p} \text{ equations}$$
Moments of Inertia for basic shapes:  
Slender Bar about COM; Slender Bar about end  

$$\frac{ml^{2}}{12} \qquad \frac{ml^{2}}{3}$$
Cylindrical Disk Sphere

$$\frac{mR^2}{2} \qquad \qquad \frac{2}{5}mR^2$$

Parallel Axis Theorem:  $I = I_G + md^2$ Radius of Gyration:  $I = mk^2$